Solution Manual for Principles of Geotechnical Engineering 9th Edition Das Sobhan 13059709349781305970939

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## Chapter 2

$2.1 \quad C_{u}=\frac{D_{60}}{D_{10}}=\frac{0.48}{0.11}=\mathbf{4 . 3 6} ; \quad C=\frac{\square_{30} D^{2}}{=} \quad \frac{0.25^{2}}{c}=\mathbf{1 . 1 8}$

Since $C_{u}>4$ and $C_{c}$ is between 1 and 3 , the soil is well graded.
$2.2 \quad C_{u}=\frac{D_{60}}{D_{10}}=\frac{1.1}{0.18}=\mathbf{6 . 1 1} ; C=\frac{\square_{30} \underline{D}^{2}}{c} \frac{0.41^{2}}{(1.1)(0.18)}=0.727 \approx \mathbf{0 . 7 3}=\left(D_{60}\right)\left(D_{10}\right)$

Although $C_{u}>6, C_{c}$ is not between 1 and 3 . The soil is poorly graded.

The $D_{10}, D_{30}$, and $D_{60}$ for soils $A, B$, and $C$ are obtained from the grain-size distribution curves.


Soil $A: \quad C_{u}=\stackrel{D_{60}}{D_{10}}=\frac{\underline{3.5}}{0.2}=\mathbf{1 7 . 5} ; C_{c}=\frac{D^{2}}{\left(D_{60}\right)\left(D_{10}\right)}=\frac{1.95^{2}}{(3.5)(0.2)}=\mathbf{5 . 4 3}$

Although $C_{u}>6, C_{c}$ is not between 1 and 3 . The sand is poorly graded.

Soil $B: \quad C_{u}=-\stackrel{D_{60}}{=-} \begin{aligned} & D_{10} \\ & = \\ & 0.17\end{aligned}=\mathbf{8 . 8 2} ; \quad C_{c}=\underset{\left(D_{60}\right)\left(D_{10}\right)}{\square_{30}}=\frac{0.75^{2}}{(1.5)(0.17)}=\mathbf{2 . 2}$
$C_{u}>6$ and $C_{c}$ is between 1 and 3 . The sand is well graded.
Soil $C: \quad C_{u}=\stackrel{D_{60}}{D_{10}}=\frac{0.55}{0.032}=\mathbf{1 7 . 2} ; \quad C_{c}=\frac{D^{2}}{\left(\square_{30}\right.}=\frac{0.22^{2}}{\left(D_{60}\right)\left(D_{10}\right)}=(0.55)(0.032)=\mathbf{2 . 7 5}$
$C_{u}>6$ and $C_{c}$ is between 1 and 3 . The sand is well graded.
2.4 a.

| Sieve <br> No. | Mass of soil retained <br> on each sieve $(\mathrm{g})$ | Percent retained <br> on each sieve | Percent <br> finer |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
| 4 | 0.0 | 0.0 | $\mathbf{1 0 0 . 0}$ |
| 10 | 18.5 | 4.4 | $\mathbf{9 5 . 6}$ |
| 20 | 53.2 | 12.6 | $\mathbf{8 3 . 0}$ |
| 40 | 90.5 | 21.5 | $\mathbf{6 1 . 5}$ |
| 60 | 81.8 | 19.4 | $\mathbf{4 2 . 1}$ |
| 100 | 92.2 | 21.9 | $\mathbf{2 0 . 2}$ |
| 200 | 58.5 | 13.9 | $\mathbf{6 . 3}$ |
| Pan | 26.5 | 6.3 | $\mathbf{0}$ |
|  | $\sum 421.2 \mathrm{~g}$ |  |  |

The grain-size distribution is shown in the figure.


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b. $D_{60}=\mathbf{0 . 4} \mathbf{~ m m} ; D_{30}=\mathbf{0 . 2} \mathbf{~ m m} ; D_{10}=\mathbf{0 . 0 9 5} \mathbf{~ m m}$
c. $\quad C_{u}=\frac{D_{60}}{D_{10}}=\frac{0.4}{0.095}=\mathbf{4 . 2 1}$
d. $\quad C_{c}=\frac{\left(D_{30}\right)^{2}}{\left(D_{10}\right)\left(D_{60}\right)} \mathbf{1 . 0 5}=\frac{(0.2)^{2}}{(0.4)(0.095)}=$
2.5 a.

| Sieve <br> No. | Mass of soil retained <br> on each sieve $(\mathrm{g})$ | Percent retained <br> on each sieve | Percent <br> finer |
| :--- | :--- | :--- | :--- |
| 4 | 0 | 0.0 | $\mathbf{1 0 0}$ |
| 6 | 30 | 6.0 | $\mathbf{9 4 . 0}$ |
| 10 | 48.7 | 9.74 | $\mathbf{8 4 . 2 6}$ |
| 20 | 127.3 | 25.46 | $\mathbf{5 8 . 8 0}$ |
| 40 | 96.8 | 19.36 | $\mathbf{3 9 . 4 4}$ |
| 60 | 76.6 | 15.32 | $\mathbf{2 4 . 1 2}$ |
| 100 | 55.2 | 11.04 | $\mathbf{1 3 . 0 8}$ |
| 200 | 43.4 | 8.68 | $\mathbf{4 . 4 0}$ |
| Pan | 22 | 4.40 | $\mathbf{0}$ |
|  | $\sum 500 \mathrm{~g}$ |  |  |

The grain-size distribution is shown in the figure.

b. $D_{10}=\mathbf{0 . 1 3} \mathbf{~ m m} ; D_{30}=\mathbf{0 . 3} \mathbf{~ m m} ; D_{60}=\mathbf{0 . 9} \mathbf{~ m m}$
c. $\quad C_{u}=\frac{D_{60}}{D_{10}}=\frac{0.9}{0.13}=\mathbf{6 . 9 2 3} \approx \mathbf{6 . 9 2}$
d. $\quad C_{c}=\frac{\sqcap_{30} D^{2}}{\left(D_{60}\right)\left(D_{10}\right)} \quad \frac{0.3^{2}}{(0.9)(0.13)}=\mathbf{0 . 7 6 9} \approx \mathbf{0 . 7 7}$
2.6 a.

| Sieve <br> No. | Mass of soil retained <br> on each sieve $(\mathrm{g})$ | Percent retained <br> on each sieve | Percent <br> finer |
| :--- | :--- | :--- | :--- |
|  |  | 0 |  |
| 4 | 0 | 7.99 | $\mathbf{1 0 0}$ |
| 10 | 44 | 10.16 | $\mathbf{9 2 . 0 1}$ |
| 20 | 56 | 14.88 | $\mathbf{8 1 . 8 5}$ |
| 40 | 82 | 9.26 | $\mathbf{6 6 . 9 7}$ |
| 60 | 51 | 19.24 | $\mathbf{5 7 . 7 1}$ |
| 80 | 106 | 16.70 | $\mathbf{3 8 . 4 7}$ |
| 100 | 92 | 15.43 | $\mathbf{2 1 . 7 7}$ |
| 200 | 85 | 5.34 | $\mathbf{6 . 3 4}$ |
| Pan | 35 |  | $\mathbf{0}$ |
|  | $\sum 551 \mathrm{~g}$ |  |  |

The grain-size distribution is shown in the figure.

b. $D_{60}=\mathbf{0 . 2 8} \mathbf{~ m m} ; D_{30}=\mathbf{0 . 1 7} \mathbf{~ m m} ; D_{10}=\mathbf{0 . 0 9 5} \mathbf{~ m m}$
c. $\quad C_{u}=\frac{0.28}{0.095}=\mathbf{2 . 9 5}$
d. $\quad C_{c}=\frac{(0.17)^{2}}{(0.095)(0.28)}=\mathbf{1 . 0 9}$
2.7 a.

| Sieve <br> No. | Mass of soil retained <br> on each sieve $(\mathrm{g})$ | Percent retained <br> on each sieve | Percent <br> finer |
| :--- | :--- | :--- | :--- |
| 4 | 0 | 0.0 | $\mathbf{1 0 0}$ |
| 6 | 0 | 0.0 | $\mathbf{1 0 0}$ |
| 10 | 0 | 0.0 | $\mathbf{1 0 0}$ |
| 20 | 9.1 | 1.82 | $\mathbf{9 8 . 1 8}$ |
| 40 | 249.4 | 49.88 | $\mathbf{4 8 . 3}$ |
| 60 | 179.8 | 35.96 | $\mathbf{1 2 . 3 4}$ |
| 100 | 22.7 | 4.54 | $\mathbf{7 . 8}$ |
| 200 | 15.5 | 3.1 | $\mathbf{4 . 7}$ |
| Pan | 23.5 | 4.7 | $\mathbf{0}$ |
|  | $\sum 500 \mathrm{~g}$ |  |  |

The grain-size distribution is shown in the figure.

b. $D_{10}=\mathbf{0 . 2 1} \mathbf{~ m m} ; D_{30}=\mathbf{0 . 3 9} \mathbf{~ m m} ; D_{60}=\mathbf{0 . 4 5} \mathbf{~ m m}$
c. $\quad C_{u}=\frac{D_{60}}{D_{10}}=\frac{0.45}{0.21}=\mathbf{2 . 1 4 2} \approx \mathbf{2 . 1 4}$
d. $\quad C_{c}=\frac{\Pi_{30} D^{2}}{\left(D_{60}\right)\left(D_{10}\right)} \frac{0.39^{2}}{(0.45)(0.21)}=\mathbf{1 . 6 0 9} \approx \mathbf{1 . 6 1}$
a. The grain-size distribution curve is shown in the figure

b. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.06 \mathrm{~mm}=84$
Percent passing $0.002 \mathrm{~mm}=11$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-84=\mathbf{1 6 \%}$
SILT: $84-11=\mathbf{7 3 \%}$
CLAY: $11-0=\mathbf{1 1 \%}$
c. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.05 \mathrm{~mm}=80$
Percent passing $0.002 \mathrm{~mm}=11$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-80=\mathbf{2 0 \%}$
SILT: $80-11=\mathbf{6 9 \%}$
CLAY: $11-0=\mathbf{1 1 \%}$
d. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.075 \mathrm{~mm}=90$
Percent passing $0.002 \mathrm{~mm}=11$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-90=\mathbf{1 0 \%}$
SILT: $90-11=79 \%$
CLAY: $11-0=\mathbf{1 1 \%}$
a. The grain-size distribution curve is shown in the figure.

b. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.06 \mathrm{~mm}=73$
Percent passing $0.002 \mathrm{~mm}=9$
GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-73=\mathbf{2 7 \%}$
SILT: $73-9=\mathbf{6 4 \%}$
CLAY: $9-0=\mathbf{9 \%}$
c. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.05 \mathrm{~mm}=68$
Percent passing $0.002 \mathrm{~mm}=9$
GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-68=\mathbf{3 2 \%}$
SILT: $68-9=\mathbf{5 9 \%}$
CLAY: $9-0=\mathbf{9 \%}$
d. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.075 \mathrm{~mm}=80$
Percent passing $0.002 \mathrm{~mm}=9$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-80=\mathbf{2 0 \%}$
SILT: $80-9=\mathbf{7 1 \%}$
CLAY: $9-0=\mathbf{9 \%}$
a. The grain-size distribution curve is shown in the figure.

b. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.06 \mathrm{~mm}=30$
Percent passing $0.002 \mathrm{~mm}=5$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-30=\mathbf{7 0 \%}$
SILT: $30-5=\mathbf{2 5 \%}$
CLAY: $5-0=\mathbf{5 \%}$
c. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.05 \mathrm{~mm}=28$
Percent passing $0.002 \mathrm{~mm}=5$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-28=\mathbf{7 2 \%}$
SILT: $28-5=\mathbf{2 3 \%}$
CLAY: 5-0=5\%
d. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.075 \mathrm{~mm}=34$
Percent passing $0.002 \mathrm{~mm}=5$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-34=\mathbf{6 6 \%}$
SILT: $34-5=\mathbf{2 9 \%}$
CLAY: $5-0=\mathbf{5 \%}$
a. The grain-size distribution curve is shown in the figure.

b. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.06 \mathrm{~mm}=65$
Percent passing $0.002 \mathrm{~mm}=35$
GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-65=\mathbf{3 5 \%}$
SILT: $65-35=\mathbf{3 0 \%}$
CLAY: $35-0=\mathbf{3 5 \%}$
c. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.05 \mathrm{~mm}=62$
Percent passing $0.002 \mathrm{~mm}=35$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-62=\mathbf{3 8 \%}$
SILT: $62-35=\mathbf{2 7 \%}$
CLAY: $35-0=\mathbf{3 5 \%}$
d. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.075 \mathrm{~mm}=70$
Percent passing $0.002 \mathrm{~mm}=35$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-70=\mathbf{3 0 \%}$
SILT: $70-35=\mathbf{3 5 \%}$
CLAY: $35-0=\mathbf{3 5 \%}$
a. The grain-size distribution curve is shown in the figure.

b. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.06 \mathrm{~mm}=96$
Percent passing $0.002 \mathrm{~mm}=42$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-96=4 \%$
SILT: $96-42=\mathbf{5 4 \%}$
CLAY: $42-0=\mathbf{4 2 \%}$
c. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.05 \mathrm{~mm}=95$
Percent passing $0.002 \mathrm{~mm}=42$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-95=\mathbf{5 \%}$
SILT: $95-42=\mathbf{5 3 \%}$
CLAY: $42-0=\mathbf{4 2 \%}$
d. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.075 \mathrm{~mm}=97$
Percent passing $0.002 \mathrm{~mm}=42$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-97=\mathbf{3 \%}$
SILT: $97-42=\mathbf{5 5 \%}$
CLAY: $42-0=\mathbf{4 2 \%}$
a. The grain-size distribution curve is shown below.

b. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.06 \mathrm{~mm}=84$
Percent passing $0.002 \mathrm{~mm}=28$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-84=\mathbf{1 6 \%}$
SILT: $84-28=\mathbf{5 6 \%}$
CLAY: $28-0=\mathbf{2 8 \%}$
c. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.05 \mathrm{~mm}=83$
Percent passing $0.002 \mathrm{~mm}=28$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-83=\mathbf{1 7 \%}$
SILT: $83-28=\mathbf{5 5 \%}$
CLAY: $28-0=\mathbf{2 8 \%}$
d. Percent passing $2 \mathrm{~mm}=100$

Percent passing $0.075 \mathrm{~mm}=90$
Percent passing $0.002 \mathrm{~mm}=28$

GRAVEL: $100-100=\mathbf{0 \%}$
SAND: $100-90=\mathbf{1 0 \%}$
SILT: $90-28=\mathbf{6 2 \%}$
CLAY: $28-0=\mathbf{2 8 \%}$
$G_{s}=2.65 ;$ temperature $=26^{\circ} \mathrm{C} ;$ time $=45 \mathrm{~min} . ; L=10.4 \mathrm{~cm}$.
Eq. (2.6): $\quad D(\mathrm{~mm})=K$
$L$ (cm)

From Table 2.9 for $G_{s}=2.65$ and temperature $=26^{\circ} \mathrm{C}, K=0.01272$
$D=0.01272 \sqrt{\frac{10.4}{45}}=\mathbf{0 . 0 0 6} \mathbf{m m}$
$G_{s}=2.75 ;$ temperature $=21^{\circ} \mathrm{C} ;$ time $=88 \mathrm{~min} . ; L=11.7 \mathrm{~cm}$
Eq. (2.6): $\quad D(\mathrm{~mm})=K$
$L(\mathrm{~cm})$
$t$ (min)

From Table 2.6 for $G_{s}=2.75$ and temperature $=21^{\circ} \mathrm{C}, K=0.01309$
$D=0.01309 \sqrt{\frac{11.7}{88}}=\mathbf{0 . 0 0 4 7} \mathbf{~ m m}$

## CRITICAL THINKING PROBLEMS

a. Soil $A: \quad C_{u}=\begin{aligned} & D_{60} \\ & D_{10}= \\ & =11 \\ & 0.6\end{aligned}=\mathbf{1 8 . 3 3} ; \quad C_{c}=\frac{D^{2}}{\square\left(D_{60}\right)\left(D_{10}\right)}=\quad \frac{5^{2}}{(11)(0.6)}=\mathbf{3 . 7 8}$

Soil B: $\quad C_{u}=-$| $D_{60}$ |  |
| :--- | :--- |
| $D_{10}=$ |  |
| 0.2 |  |$=\mathbf{3 5} ; \quad C_{c}=\frac{D^{2}}{\square\left(D_{60}\right)\left(D_{10}\right)}=\frac{2.1^{2}}{(7)(0.2)}=\mathbf{3 . 1 5}$

Soil $C: \quad C_{u}=-\begin{aligned} & D_{60} \\ & D_{10}\end{aligned}=\begin{aligned} & \underline{4.5} \\ & 0.15\end{aligned}=\mathbf{3 0} ; \quad C_{c}=\begin{aligned} & \square_{30} \\ & \left(D_{60}\right)\left(D_{10}\right) \\ & =\end{aligned} \frac{1^{2}}{(4.5)(0.15)}=\mathbf{1 . 4 8}$
b. Soil $A$ is coarser than Soil $C$. A higher percentage of soil $C$ is finer than any given size compared to Soil $A$. For example, about $15 \%$ is finer than 1 mm for Soil $A$, whereas almost $30 \%$ is finer than 1 mm for Soil $C$.
c. Particle segregation may take place in aggregate stockpiles such that there is a separation of coarser and finer particles. This makes representative sampling difficult. Therefore, Soils $A, B$, and $C$ demonstrate quite different particle size distribution.

## d. $\underline{\text { Soil } A}$

Percent passing $4.75 \mathrm{~mm}=29$
Percent passing $0.075 \mathrm{~mm}=1$

GRAVEL: $100-29=\mathbf{7 1 \%}$
SAND: $29-1=\mathbf{2 8 \%}$
FINES: $1-0=\mathbf{1 \%}$

Soil B
Percent passing $4.75 \mathrm{~mm}=45$ GRAVEL: $100-45=\mathbf{5 5 \%}$
Percent passing $0.075 \mathrm{~mm}=2 \quad$ SAND: $45-2=\mathbf{4 3 \%}$
FINES: $2-0=\mathbf{2 \%}$
$\underline{\text { Soil } C}$
Percent passing $4.75 \mathrm{~mm}=53$ GRAVEL: $100-53=\mathbf{4 7 \%}$
Percent passing $0.075 \mathrm{~mm}=3$ SAND: $53-3=\mathbf{5 0 \%}$
FINES: $3-0=\mathbf{3 \%}$
a. Total mass in the ternary mix $=8000 \times 3=24,000 \mathrm{~kg}$

Percent of each soil in the mix $=\frac{8,000}{24,000} \times 100=33.33 \%$
Mass of each soil used in the sieve analysis, $\sum m_{A}=\sum m_{B}=\sum m_{C}=500 \mathrm{~g}$
If a sieve analysis is conducted on the ternary mix using the same set of sieves, the percent of mass retained on each sieve, $m_{M}(\%)$, can be computed as follows:


The calculated values are shown in the following table.

| Sieve size <br> (mm) |  | Mass retained |  | $\begin{array}{r} n_{M} \\ (\%) \\ \hline \end{array}$ | Percent passing for the mixture |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & m_{A} \\ & (\mathrm{~g}) \end{aligned}$ | $\begin{gathered} m_{B} \\ (\mathrm{~g}) \\ \hline \end{gathered}$ | $m_{C}$ <br> (g) |  |  |
| 25.0 | 0.0 | 0 | 0 | 0.0 | 100 |
| 19.0 | 60 | 10 | 30 | 6.66 | 93.34 |
| 12.7 | 130 | 75 | 75 | 18.65 | 74.69 |
| 9.5 | 65 | 80 | 45 | 12.65 | 62.04 |
| 4.75 | 100 | 165 | 90 | 23.64 | 38.4 |
| 2.36 | 50 | 25 | 65 | 9.32 | 29.08 |
| 0.6 | 40 | 60 | 75 | 11.65 | 17.43 |
| 0.075 | 50 | 70 | 105 | 14.98 | 2.45 |
| Pan | 5 | 15 | 15 | 2.33 | $\approx 0$ |

b. The grain-size distribution curve for the mixture is drawn below.


From the curve, $D_{10}=0.21 ; D_{30}=2.5 ; D_{60}=9.0$

$$
\begin{array}{cclcl}
C=- & D_{60}= & \underline{9.0}=\mathbf{4 2 . 8 5} ; & C=\frac{\square 30}{} \underline{D}^{2} & -\underline{2.5}^{2} \\
{ }^{u} & D_{10} & 0.21 & c & \left(D_{60}\right)\left(D_{10}\right) \\
= & (9.0)(0.21)
\end{array}
$$

